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# An LMI Approach to Static Output Feedback Stabilization of Linear Systems\*

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Abstract: In this paper, a linear matrix inequality (LMI) approach without constraints is developed to solve W- and P-problems, which are related to designing static output feedback (SOF) stabilization controls for linear systems. As an application, the SOF stabilization problem of uncertain systems is considered. Some LMI-based sufficient and necessary conditions and design approaches are presented.

Key words: LMI; static output feedback; uncertainty

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# 线性系统静态输出反馈镇定的 LMI 方法

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摘要:利用无约束条件的线性矩阵不等式(LMI)研究了W-问题和P-问题,而后者的解可用来设计静态输出反馈(SOF)镇定控制,作为一个应用考虑了不确定系统的静态输出反馈问题,给出了依赖于LMI条件的SOF设计方法。

关键词:线性矩阵不等式;静态输出反馈;不确定性

### 1 Introduction

The design of static output feedback (SOF) stabilization controllers for either certain or uncertain systems is one of the most basic and important, control problems. Although various approaches have been proposed, the analytical or numerical solution is still hard to get in general. The difficulty is that designing an SOF stabilization controller is actually equivalent to solving a set of bilinear matrix inequalities (BMIs), which are nonconvex in general, and therefore, difficult to deal with<sup>[1,2]</sup>. Recently, some efforts have been made to identify some special cases in which the solvability of the BMIs can be transferred into that of a set of linear matrix inequalities (LMIs) which can numerically be solved by LMI Toolbox<sup>[3]</sup>. For instance, under some sufficient conditions, it is shown<sup>[4]</sup> that the SOF stabilization problem is solvable if so is the so-called W-or P-problems expressed in terms LMIs and linear matrix equality (LME) constraints. However, it is still an open problem either to find the feasible conditions of or to construct a solution for a set of LMIs with an LME constraint.

The purpose of this paper is to provide some sufficient and necessary conditions for the feasibilities of both W- and P-problems, and formulate the conditions in terms of pure LMIs (i.e., without LME or any other constraint). In addition, an effective method for designing SOF stabilization controllers is given. As an application of the ideas and methods, we reconsider the SOF stabilization problem of systems with polytopic uncertainties, and essentially generalize the results of Reference [5].

Throughout this paper, the following notations are used.  $A^{T}$  is the transpose of a matrix A. A > 0 (A < 0) means A is positive (negative) definite. And for an  $n \times m$  full column rank matrix A,  $A^{\perp}$  denotes an  $(n-m) \times n$  matrix with the following properties:  $A^{\perp} A = 0_{(n-m)\times m}$  [ $A A^{\perp T}$ ]  $\in \mathbb{R}^{n\times n}$  is invertible and  $A^{\perp} A^{\perp T} = I_{(n-m)\times(n-m)}$ .

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### 2 LMI approaches to the W- and P-problems

Consider linear time-invariant system

$$\begin{cases} \dot{x} = Ax + Bu, \\ \gamma = Cx, \end{cases} \tag{1}$$

where  $x \in \mathbb{R}^n$ ,  $u \in \mathbb{R}^m$  and  $y \in \mathbb{R}^p$  are system state, input and measured output, and  $A \in \mathbb{R}^{n \times n}$ ,  $B \in \mathbb{R}^{m \times m}$  and  $C \in \mathbb{R}^{p \times n}$  are state, input and output matrices, respectively.

By SOF controls of system (1) we mean the controls of the form  $u = -L_Y(t)$  with L an  $m \times p$  constant matrix. And by SOF stabilization controls of system (1) we mean such SOF controls that stabilize the system or, equivalently, such that A = BLC is stable.

Related to this problem is the following W- and P-problems<sup>[4]</sup>:

**Definition 1** W-Problem: Given matrices A, B, C, with C full row rank the W-problem includes finding, if possible, matrices W, M, N such that

$$\begin{cases} AW + WA' - BNC - C'N'B' < 0, \\ W > 0, MC = CW. \end{cases}$$
 (2)

From [4], if (W, M, N) is a solution of the W-problem, then  $u = NM^{-1}\gamma$  is an SOF stabilization control of system (1).

**Definition 2** P-problem: Given matrices A, B, C, with B full column rank, the P-problem includes finding, if possible, matrices P, M, N such that

$$\begin{cases}
PA + A'P - BNC - C'N'B' < 0, \\
P > 0, BM = PB.
\end{cases}$$
(3)

Similarly, if (P, M, N) is a solution of the P-problem, then  $u = -M^{-1}Ny$  is also an SOF stabilization control of system (1).

For the convenience of citation, we introduce the following lemma.

**Lemma 1**<sup>{6}</sup> Suppose  $D \in \mathbb{R}^{n \times q}$  and  $E \in \mathbb{R}^{n \times q}$  are full column rank. Then there exists an  $n \times n$  positive definite matrix P such that PD = E if and only if  $D^TE = E^TD > 0$ . Furthermore, all solutions of PD = E can be expressed as

$$P = E(D^{T}E)^{-1}E^{T} + D^{\perp T}XD^{\perp}, \qquad (4)$$

where  $X \in \mathbb{R}^{(n-q)\times (n-q)}$  is an arbitrary positive definite matrix.

**Theorem 1** Suppose C is full row rank. Then W-problem is feasible if and only if there exist matrices X > 0, V > 0 and  $N \in \mathbb{R}^{m \times p}$  such that

$$AC_0VC_0^{\mathsf{T}} + C_0VC_0^{\mathsf{T}}A^{\mathsf{T}} + AC^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp} +$$

$$C^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp}A^{\mathsf{T}} - BNC - C^{\mathsf{T}}N^{\mathsf{T}}B^{\mathsf{T}} < 0. \tag{5}$$

where  $C_0 = C^{T}(CC^{T})^{-1}$ . Furthermore, when (5) holds, system (1) is stabilized by SOF control law  $u = -NCC^{T}V^{-1}\gamma$ .

Proof Suppose that there exist matrices X > 0, V > 0 and  $N \in \mathbb{R}^{m \times p}$  satisfying (5). Let  $M = V(CC^T)^{-1}$ . Then we have

$$CC^{\mathsf{T}}M^{\mathsf{T}} = MCC^{\mathsf{T}} > 0, (6)$$

and

$$AC_0MC + C^{\mathsf{T}}M^{\mathsf{T}}C_0^{\mathsf{T}}A^{\mathsf{T}} + AC^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp} + C^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp}A^{\mathsf{T}} - BNC - C^{\mathsf{T}}N^{\mathsf{T}}B^{\mathsf{T}} < 0.$$
 (7)

From (6) and Lemma 1,  $WC^T = C^T M^T$  has a positive definite matrix solution W, which can be expressed in the form of

$$W = C_0 M C + C^{T \perp T} X C^{T \perp}. \tag{8}$$

where X is a positive definite matrix. Substituting (8) into (7) leads to the first inequality of (2). Thus, the W-problem is feasible.

Conversely, assume that W-problem is feasible. Let  $V = M(CC^{T})$ . Then the result can be easily implied in terms of Lemma 1.

This completes the proof.

Remark 1 The same approach as Theorem 1 can also easily be used to discuss P-problem and similar results can be obtained.

Remark 2 The presented approach can also easily be used to design SOF stabilization controls for discrete-time linear systems, decentralized output feedback control, output feedback  $H_{\varpi}$  control, and other related control problems described, for instance, in [4].

# 3 Application to uncertain systems

In this section, by using the approaches developed in Section 2 we consider the SOF stabilization problem of systems with polytopic uncertainties:

$$\begin{cases} \dot{x} = Ax + Bu \text{ with } (A, B) \in \Omega \underline{\triangle} \\ \{(A, B) : (A_1, B_1), \dots, (A_k, B_k)\}, \quad (9) \\ y = Cx, \end{cases}$$

where  $x \in \mathbb{R}^n$  is the state vector,  $u \in \mathbb{R}^m$  the input and  $\gamma \in \mathbb{R}^p$  the output.

The system (9) actually represents a family of multiinput and multi-output systems, and is very different from the matched uncertain ones, which admits a nominal system and matched uncertainties. To our knowledge, the first progress on the SOF stabilization of system (9) was made by Kar in [5], the following three assumptions  $i \sim iii$  were imposed and the simultaneously quadratically (SQ) stabilizable concept was adopted.

**Assumption i** There are B and  $G_i$  such that  $B_i = BG_i$ , where  $G_i \in \mathbb{R}^{m \times m}$  is nonsingular and satisfies  $G_i + G_i^T > 0$  for all  $i = 1, \dots, k$ .

**Assumption ii** The number of control inputs is equal to the number of measurable outputs, i.e., p = m. The matrices B and C are of the form:  $B = \begin{bmatrix} 0 & I_m \end{bmatrix}^T$ ,  $C = \begin{bmatrix} C_1 & C_2 \end{bmatrix}$ , where  $C_2 \in \mathbb{R}^{m \times m}$  is non-singular.

**Assumption iii** The transfer function matrix  $C(sI_n - A_i)^{-1}B_i$  for each system is strictly minimum phase, i. e., all the zeros of the system lie in the open left half of the complete plane.

**Definition 3** System (9) is simultaneously quadratically (SQ) stabilizable via an SOF control: u = -Ly if there exist a positive definite matrix Q and a matrix L such that

$$(A_i - B_i LC)^{\mathsf{T}} Q^{-1} + Q^{-1} (A_i - B_i LC) < 0, \quad \forall \ i = 1, \dots, k.$$
(10)

Suppose there are B and  $G_i$  such that  $B_i = BG_i$  ( $i = 1, \dots, k$ ). Then it is obvious that if there exist a positive definite matrix Q, a nonsingular matrix L and a positive scalar  $\gamma$  such that

$$A_{i}Q + QA_{i}^{T} - \frac{1}{2}\gamma(B_{i}B^{T} + BB_{i}^{T}) < 0, \ \forall i = 1, \dots, k,$$

$$(11)$$

and

$$LC = \frac{1}{2} \gamma B^{\mathsf{T}} Q^{-1}, \tag{12}$$

then system (9) is SQ stabilized by the SOF control  $u = -L\gamma$ .

**Theorem 2**<sup>[5]</sup> Suppose that Assumptions  $i \sim iii$  hold. Then there exist a positive definite matrix Q and a matrix L such that (11) and (12) hold for some positive  $\gamma$  if and only if there exists a positive definite matrix  $W_1$  such that

$$(A_{11}^{i} - A_{12}^{i}F) W_{1} + W_{1}(A_{11}^{i} - A_{12}^{i}F)^{T} < 0, \forall i = 1, \dots, k.$$
(13)

where  $F=C_2^{-1}C_1$ , and  $A_{11}^i\in\mathbb{R}^{(n-m)\times(n-m)}$  and  $A_{12}^i\in$ 

$$\mathbb{R}^{(n-m)\times m}$$
 are parts of  $A_i$  and defined by  $\begin{bmatrix} A_{11}^i & A_{12}^i \\ A_{21}^i & A_{22}^i \end{bmatrix} \triangleq A_i$ .

In order to apply the approaches developed in Section 2, we now revisit the SOF stabilization problem of system (9), weaken the assumptions in [5]. To this end, we introduce the following assumptions:

**Assumption a** There are B and  $G_i$  such that  $B_i = BG_i$  with  $G_i \in \mathbb{R}^{m \times m}$  for all  $i = 1, \dots, k$ .

**Assumption b** CB is square and nonsingular.

Obviously, Assumptions a and b are weaker than Assumptions i and ii, especially in the sense that the positive definite condition on matrix  $G_i + G_i^T$  (for all i = 1, ..., k) and the special structure condition on B and C are not required.

According to Lemma 1, there exists a positive definite matrix Q satisfying (12) if and only if there must be  $L(CB) = (CB)^{T}L^{T} > 0$ , and Q can be expressed as

$$Q = \frac{1}{2} \gamma B (LCB)^{-1} B^{\mathsf{T}} + (LC)^{\mathsf{T}_{\perp} \mathsf{T}} X (LC)^{\mathsf{T}_{\perp}},$$

Let  $\frac{1}{2}\gamma(LCB)^{-1} = N$ . Then similar to Theorem 1, we can show the following theorem.

Theorem 3 Suppose the assumptions a and b hold. Then there exist a positive definite matrix Q, a matrix L and a positive scalar  $\gamma$  such that (11) and (12) hold if and only if there exist matrices X > 0, N > 0 and a positive scalar constant  $\gamma$  such that

$$A_{i}BNB^{\mathsf{T}} + BNB^{\mathsf{T}}A_{i}^{\mathsf{T}} + A_{i}C^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp} + C^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp}A_{i}^{\mathsf{T}} - \frac{1}{2}\gamma(B_{i}B^{\mathsf{T}} + BB_{i}^{\mathsf{T}}) < 0 \quad (14)$$

hold for  $i = 1, 2, \dots, k$ . Furthermore, system (9) is SQ stabilizable by the SOF control  $u = -\frac{y}{2}(CBN)^{-1}y$ .

**Remark 3** In addition to a and b, if  $G_i + G_i^T > 0$  for  $i = 1, \dots, k$ , then we can directly, without using (11) and (12), show that there exist matrices X > 0, N > 0 and a positive scalar constant  $\gamma$  such that (14) holds for  $i = 1, 2, \dots, k$ , if and only if there exists a positive definite matrix  $W_1$  such that (13) holds.

To do so, let's partition  $C^{T\perp}$  in the form  $[C_3 C_4] = C^{T\perp}$ , where  $C_3 \in \mathbb{R}^{(n-m)\times (n-m)}$  and  $C_4 \in \mathbb{R}^{(n-m)\times m}$ . Then

$$C_3 C_1^{\mathrm{T}} + C_4 C_2^{\mathrm{T}} = 0_{(n-m)\times m},$$
  
 $C_3 C_3^{\mathrm{T}} + C_4 C_4^{\mathrm{T}} = 0_{(n-m)\times (n-m)},$ 

which is equivalent to

$$C_4 = -C_3(C_2^{-1}C_1)^T = -C_3F^T$$
 (15)

and

$$C_3(I_{(n-m)\times(n-m)} + F^T F) C_3^T = I_{(n-m)\times(n-m)},$$
(16)

respectively, where  $F = C_2^{-1}C_1 \in \mathbb{R}^{m \times (n-m)}$ . By (16)  $C_3$  is nonsingular, and by (15),

$$C^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp} = \begin{bmatrix} C_3^{\mathsf{T}} \\ -FC_3^{\mathsf{T}} \end{bmatrix} X \begin{bmatrix} C_3 & -C_3F^{\mathsf{T}} \end{bmatrix} = \begin{bmatrix} C_3^{\mathsf{T}}XC_3 & -C_3^{\mathsf{T}}XC_3F^{\mathsf{T}} \\ -FC_3^{\mathsf{T}}XC_3 & FC_3^{\mathsf{T}}XC_3F^{\mathsf{T}} \end{bmatrix}.$$
(17)

Let  $W_1 = C_3^T X C_3$ . Then it is obvious that X > 0 if and only if  $W_1 > 0$ . Substituting (17) into (14), it can be seen that (14) hold if and only if the following inequalities hold:

$$A_{i} \begin{bmatrix} W_{1} & -W_{1}F^{T} \\ -FW_{1} & FW_{1}F^{T} + N \end{bmatrix} + \begin{bmatrix} W_{1} & -W_{1}F^{T} \\ -FW_{1} & FW_{1}F^{T} + N \end{bmatrix} A_{i}^{T} - \frac{1}{2}\gamma \begin{bmatrix} 0 & 0 \\ 0 & G_{i} + G_{i}^{T} \end{bmatrix} < 0.$$
(18)

And (18) is equivalent to (13) in the case where  $G_i + G_i^T > 0$  for  $i = 1, \dots, k$ . This implies the result of Remark 3.

Similar to Theorem 1, we can get the following results for uncertain systems of the form (9).

**Theorem 4** Suppose C is full row rank. If there exist matrices X > 0, N > 0 and  $Y \in \mathbb{R}^{m \times p}$  such that

$$A_{i}C_{0}NC_{0}^{\mathsf{T}} + C_{0}NC_{0}^{\mathsf{T}}A_{i}^{\mathsf{T}} + A_{i}C^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp} + C^{\mathsf{T}\perp\mathsf{T}}XC^{\mathsf{T}\perp}A_{i}^{\mathsf{T}} - B_{i}YC - C^{\mathsf{T}}Y^{\mathsf{T}}B_{i}^{\mathsf{T}} < 0, \quad (19)$$

for  $i = 1, 2, \dots, l$ , where  $C_0 = C^{T}(CC^{T})^{-1}$ , then system (9) is stabilized by SOF control  $u = -YCC^{T}N^{-1}\gamma$ .

Remark 4 Compared with Theorems 2 and 3, Theorem 4 does not require any of Assumptions i and iii or a,b. This essentially weakens the conditions of Theorems 2 and 3. In the following section, we will give an example to illustrate this.

### 4 Example

**Example 1** Consider an uncertain system (9) with  $(A,B) = (A_1,B_1)$ , or  $(A_2,B_2)$ , where

$$A_{1} = \begin{bmatrix} -2 & 0 & 2 \\ 0 & 0 & 1 \\ 0 & -1 & 0 \end{bmatrix}, A_{2} = \begin{bmatrix} -1 & 2 & -3 \\ 0 & -2 & 1 \\ 1 & 0 & -3 \end{bmatrix},$$

$$B_{1} = \begin{bmatrix} 1 \\ -1 \\ 0 \end{bmatrix}, B_{2} = \begin{bmatrix} -1 \\ 0 \\ 1 \end{bmatrix}, C = \begin{bmatrix} 0 & 1 & 1 \end{bmatrix}.$$

By a straightforward calculation, it is easy to see that  $C(sI - A_1)^{-1}B_1 = \frac{-s+1}{s^2+1}$ . This means that the zero of system  $\dot{x} = A_1x + B_1u$  is 1, in the right half of the complex plane. And so, Assumption iii is not satisfied

and by Remark 3, the results of Theorems 2 and 3 cannot be applied to this example. But by using Theorem 4, we can give an SOF stabilization control  $u = 0.7998\gamma$ .

#### 5 Conclusion

In this paper, a pure linear matrix inequality approach (i.e. without linear matrix equality or any other constraint) is developed to solve the W-and P-problems, which are related to designing SOF stabilization controls for linear systems. As an application of the approach, the SOF stabilization problem of linear systems with polytopic uncertainties is considered. Some LMI-based conditions and design approaches are presented, which not only essentially generalizes the existing results (e.g. [5]) but are also easily solved. In addition, our approach can also easily be used to design SOF stabilization controls for discrete-time linear systems, decentralized output feedback control, output feedback  $H_{\infty}$  control, and other related control problems described for instance, in [4].

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