

线性离散时滞系统的鲁棒耗散控制

邵汉永

(曲阜师范大学 电气信息与自动化学院, 山东 日照 276826)

摘要: 考虑线性离散时滞系统的二次型耗散控制问题. 对于确定系统, 给出渐近稳定且严格二次型耗散的条件和动态输出反馈控制器使闭环系统渐近稳定且严格二次型耗散. 对于不确定系统, 考虑不确定性具有耗散特性的情形, 讨论鲁棒耗散性分析和动态输出反馈鲁棒耗散控制问题. 通过构造增广系统, 将不确定系统的鲁棒严格二次型耗散分析和设计转化为确定系统的情况. 所得结果为离散时滞系统的无源控制和 H_∞ 控制提供了统一框架, 且为离散时滞系统的分析和设计提供了一种更灵活、保守性更小的方法.

关键词: 离散时滞系统; 二次型耗散性; 耗散控制; LMI

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Robust dissipative control for a class of uncertain linear discrete-time systems with time-delay

SHAO Han-yong

(College of Electric, Information and Automation, Qufu Normal University, Rizhao Shandong 276826, China)

Abstract: Quadratic-dissipative control for linear discrete-time systems with time-delay is considered in this paper. Firstly, for the system without uncertainties, conditions are characterized for the systems to be asymptotically stable and strictly quadratic-dissipative. The output feedback dissipative control problem is then addressed, and methods for designing those controllers are also given. Secondly, as for uncertain systems, the considered structured uncertainty is characterized by a dissipative system. Robust quadratic-dissipative analysis is addressed. Dynamic output feedback controllers are developed so that the closed-loop system will achieve robust stability and strictly quadratic dissipativeness. Finally, the robust dissipative analysis and synthesis are respectively reduced to the dissipative analysis and synthesis problems without uncertainties. Results of the output feedback dissipative control can provide not only a unified framework for H_∞ control and passive control but also a more flexible and less conservative design for linear discrete-time systems with time-delay.

Key words: discrete-time systems with delay; quadratic dissipativeness; dissipative control; LMI

1 引言 (Introduction)

耗散性是系统和控制理论中的一个重要概念, 它在稳定性分析、非线性控制及自适应控制系统设计等方面有广泛应用^[1,2], 它是无源概念及 H_∞ 性能的推广. 近年来无源控制及 H_∞ 控制成为许多学者研究的热点问题^[3-5,7], 然而, 无源设计由于只提取了相位信息, 所得结果有较大保守性. H_∞ 控制则只利用了系统的增益, 所得结果也有较大保守性. 而基于耗散性的综合由于既利用了系统的增益又提取了相位信息, 在增益和相位之间进行了较好的折中, 所得结果保守性较小. 因此, 研究系统的耗散性具有重要意义. 近几年由于 H_∞ 理论的发展, 线性系统的二

次型耗散问题得到进一步研究. 文[8]讨论了线性连续系统的二次型耗散控制问题, 文[9]则给出了线性离散系统的二次型耗散控制器. 由于时滞现象在实际系统中普遍存在, 时滞系统的二次型耗散控制近来成为一个研究热点. 线性时滞系统的 H_∞ 控制已得到广泛研究^[10,11], 而文[12]则讨论了线性时滞系统的无源控制问题. 然而, 对于时滞系统的一般耗散问题, 现有文献讨论得还很不够. 文[13]对线性连续时滞系统考虑了严格二次型耗散控制, 给出了控制器的存在条件与综合方法. 至于线性离散时滞系统, 文[14]只考虑了状态方程中有时滞的情形, 而且只研究了状态反馈耗散控制问题.

本文就状态方程和输出方程均有时滞的线性离散时滞系统,考虑严格二次型耗散的分析 and 输出反馈控制问题.在确定系统的基础上引入耗散不确定性,研究不确定离散时滞系统的鲁棒耗散性分析和动态输出反馈鲁棒耗散控制.

2 基础知识 (Preliminaries)

为研究线性离散系统的鲁棒耗散性分析和控制问题,先给出必要的基础知识.考虑下面的线性离散时滞系统

$$\begin{cases} x(k+1) = Ax(k) + A_d x(k-d) + B_1 w(k) + B_2 u(k), \\ z(k) = C_1 x(k) + C_{1d} x(k-d) + D_{11} w(k) + D_{12} u(k), \\ y(k) = C_2 x(k) + C_{2d} x(k-d) + D_{21} w(k), \\ x(k) = x_0(k), -d \leq k \leq 0. \end{cases} \quad (1)$$

其中: $x \in \mathbb{R}^n$ 为状态, $w \in \mathbb{R}^q$ 为外部输入, $z \in \mathbb{R}^p$ 为被控输出, $y \in \mathbb{R}^r$ 为量测输出, $u \in \mathbb{R}^m$ 为控制输入, $x_0(k) (-d \leq k \leq 0)$ 为初始条件. $A, A_d, D_{12}, B_i, C_i, C_{id}, D_{i1} (i = 1, 2)$ 为适当维数的已知矩阵.

令 $u(k) = 0$, 从系统(1)得

$$\begin{cases} x(k+1) = Ax(k) + A_d x(k-d) + B_1 w(k), \\ z(k) = C_1 x(k) + C_{1d} x(k-d) + D_{11} w(k), \\ x(k) = x_0(k), -d \leq k \leq 0. \end{cases} \quad (2)$$

给定适当维数的矩阵 Q, S, R (Q, R 是对称的), 使

$$A1) Q \leq 0,$$

$$A2) R + D_{11}^T S + S^T D_{11} + D_{11}^T Q D_{11} > 0.$$

于是有

定理 1^[6] 设 $-Q$ 的满秩分解为 $L^T L$. 若存在 $P > 0, W > 0$ 使

$$\begin{bmatrix} -P + W & * & * & * & * \\ 0 & -W & * & * & * \\ -S^T C_1 & -S^T C_{1d} & -D_{11}^T S - S^T D_{11} - R & * & * \\ PA & PA_d & PB_1 & -P & * \\ LC_1 & LC_{1d} & LD_{11} & 0 & -I \end{bmatrix} < 0,$$

则系统(2)渐近稳定且严格 (Q, S, R) -耗散. 记

$$\Psi_1 = \begin{bmatrix} \phi_{11} & * & * & * \\ 0 & -W & * & * \\ \phi_{13}^T & -S^T C_{1d} & -D_{11}^T S - S^T D_{11} - R & * \\ \phi_{14}^T & \phi_{24}^T & \phi_{34}^T & \phi_{44} \end{bmatrix},$$

$$\Psi_2^T = \begin{bmatrix} \phi_{15}^T & LC_{1d} & LD_{11} & 0 \\ \phi_{16}^T & 0 & 0 & 0 \end{bmatrix}, \quad \Psi_3 = - \begin{bmatrix} I & 0 \\ 0 & W^{-1} \end{bmatrix},$$

$$\phi_{11} = \begin{bmatrix} -X & -I + XW \\ -I + WX & -Y + W \end{bmatrix},$$

$$\phi_{14}^T = - \begin{bmatrix} AX + B_2 G & A \\ H & YA + FC_2 \end{bmatrix},$$

$$\phi_{24}^T = \begin{bmatrix} A_d \\ YA_d + FC_{2d} \end{bmatrix}, \quad \phi_{34}^T = \begin{bmatrix} B_1 \\ YB_1 + FD_{21} \end{bmatrix},$$

$$\phi_{44} = - \begin{bmatrix} X & I \\ I & Y \end{bmatrix}, \quad \phi_{13}^T = -S^T [C_1 X + D_{12} G \quad C_1],$$

$$\phi_{15}^T = L [C_1 X + D_{12} G \quad C_1], \quad \phi_{16}^T = [X \quad 0].$$

则有

定理 2^[6] 若对某矩阵 $W > 0$, 下面的矩阵不等式

$$\begin{bmatrix} \Psi_1 & \Psi_2 \\ \Psi_2^T & \Psi_3 \end{bmatrix} < 0 \quad (3)$$

关于 $Y > 0, X > 0, F, G, H$ 有可行解, 则系统(1)存在 n 阶输出反馈控制器

$\xi(k+1) = A_c \xi(k) + B_c y(k), u(k) = C_c \xi(k)$, 使闭环系统渐近稳定且严格 (Q, S, R) -耗散, 而 A_c, B_c, C_c 满足:

$$MN^T = I - XY, \quad (4)$$

$$\begin{cases} F = NB_c, G = C_c M^T, \\ H = YAX + YB_2 G + FC_2 X + NA_c M^T. \end{cases} \quad (5)$$

3 鲁棒耗散分析 (Robust dissipative analysis)

在系统(2)中引入不确定变量, 得

$$\begin{cases} x(k+1) = Ax(k) + A_d x(k-d) + B_1 w(k) + H_1 \xi(k), \\ z(k) = C_1 x(k) + C_{1d} x(k-d) + D_{11} w(k) + H_2 \xi(k), \\ \sigma(k) = E_1 x(k) + E_{1d} x(k-d) + E_2 w(k) + J \xi(k), \\ x(k) = x_0(k), -d \leq k \leq 0. \end{cases} \quad (6)$$

其中: $H_1, H_2, E_1, E_{1d}, E_2, J$ 为适当维数的已知矩阵, $\xi(k) \in \mathbb{R}^{n_1}, \sigma(k) \in \mathbb{R}^{n_2}$ 为不确定变量且具有以下二次型耗散不确定性

$$\xi^T(k) Q_0 \xi(k) + 2\xi^T(k) S_0 \sigma(k) + \sigma^T(k) R_0 \sigma(k) \geq 0, \quad \forall k \geq 0, \quad (7)$$

而 Q_0, S_0, R_0 为已知矩阵且 Q_0, R_0 为对称的. 对于 Q_0, S_0, R_0 作以下假设:

$$A3) Q_0 + S_0 J + J^T S_0^T + J^T R_0 J < 0,$$

$$A4) R_0 \geq 0.$$

注 1 假设 A3) 保证了当 $w(k) = x_0(k) = 0$ 时,

$\xi(k) \equiv 0$. 因为此时 $\sigma(k) = J\xi(k)$, 一方面, 由(7)得

$$\xi^T(k)(Q_0 + S_0J + J^TS_0^T + J^TR_0J)\xi(k) \geq 0, \forall k.$$

另一方面, 由假设 A3)得

$$\xi^T(k)(Q_0 + S_0J + J^TS_0^T + J^TR_0J)\xi(k) \leq 0, \forall k.$$

从而 $\xi(k) \equiv 0$.

所以 $x_0(k) = 0$ 为系统(6)所对应自由系统(令 $w(k) = 0$ 所得系统)的平衡状态.

注2 二次型耗散不确定性是范数有界不确定性或正实不确定性的推广. 范数有界不确定性只考虑了不确定性的增益, 正实不确定性只考虑了不确定性的相位, 这两种不确定性描述保守性较大. 二次型不确定性既包含了不确定性的增益又包含了不确定性的相位信息, 为不确定描述提供了灵活而保守性较小的方式.

注3 系统(6)不仅本身代表了一类非线性系统, 而且也包含了常见的范数有界参数不确定系统和正实参数不确定系统. 如下面的参数不确定系统

$$x(k+1) = A_\Delta x(k) + B_\Delta \omega(k), \quad z(k) = C_\Delta x(k) + D_\Delta \omega(k),$$

其中: $x(k) \in \mathbb{R}^n$ 为状态, $\omega(k) \in \mathbb{R}^q$ 为外部输入, $z(k) \in \mathbb{R}^q$ 为输出, $A_\Delta, B_\Delta, C_\Delta, D_\Delta$ 为不确定性矩阵且满足以下假设

$$\begin{bmatrix} A_\Delta & B_\Delta \\ C_\Delta & D_\Delta \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} - \begin{bmatrix} H_1 \\ H_2 \end{bmatrix} \Delta(k) \begin{bmatrix} E_1 & E_2 \end{bmatrix}.$$

$\Delta(k)$ 由不确定矩阵 $F(k)$ 决定

$$\Delta(k) = F(k)[I + JF(k)]^{-1}.$$

当 $F^T(k)F(k) \leq I$, 该系统为范数有界参数不确定系统, 显然它是系统(6)在

$$A_d = C_{1d} = E_{1d} = 0, \quad \xi(k) = -F\sigma(k),$$

$$Q_0 = -R_0 = -I, \quad S_0 = 0$$

时的特例; 当 $F^T(k) + F(k) \geq 0$, 它为正实参数不确定系统, 易见它是系统(6)在

$$A_d = C_{1d} = E_{1d} = 0, \quad \xi(k) = -F\sigma(k),$$

$$Q_0 = R_0 = 0, \quad S_0 = I$$

时的特例.

下面讨论系统(6)何时对任意不确定性(7)都是渐近稳定且严格 (Q, S, R) -耗散的, 此时称系统(6)为鲁棒稳定且严格 (Q, S, R) -耗散的. 为便于叙述分析结果, 在定理1的基础上先给出以下定义

定义 设 $-Q$ 的满秩分解为 $L^T L$. 若存在 $P > 0, W > 0$ 使

$$\Pi := \begin{bmatrix} -P + W + A^T P A & * & * & * \\ A_d^T P A & -W + A_d^T P A_d & * & * \\ B_1^T P A & B_1^T P A_d & B_1^T P B_1 & * \\ \lambda^{1/2} H_1^T P A & \lambda^{1/2} H_1^T P A_d & \lambda^{1/2} H_1^T P B_1 & \lambda H_1^T P H_1 \end{bmatrix} +$$

$$\begin{bmatrix} -P + W & * & * & * & * \\ 0 & -W & * & * & * \\ -S^T C_1 & -S^T C_{1d} & -D_{11}^T S - S^T D_{11} - R & * & * \\ P A & P A_d & P B_1 & -P & * \\ L C_1 & L C_{1d} & L D_{11} & 0 & -I \end{bmatrix} < 0,$$

则称系统(2)二次稳定且严格 (Q, S, R) -耗散的.

引进下面的增广系统

$$\begin{cases} x(k+1) = Ax(k) + A_d x(k-d) + B_{1\lambda} \bar{w}(k) =: \\ \quad Ax(k) + A_d x(k-d) + \\ \quad [B_1 \quad \lambda^{1/2} H_1] \bar{w}(k), \\ \bar{z}(k) = C_{1\lambda} x(k) + C_{1d\lambda} x(k-d) + D_{11\lambda} \bar{w}(k) =: \\ \quad \begin{bmatrix} C_1 \\ \lambda^{-1/2} E_1 \end{bmatrix} x(k) + \begin{bmatrix} C_{1d} \\ \lambda^{-1/2} E_{1d} \end{bmatrix} x(k-d) + \\ \quad \begin{bmatrix} D_{11} & \lambda^{1/2} H_2 \\ \lambda^{-1/2} E_2 & J \end{bmatrix} \bar{w}(k). \end{cases} \quad (8)$$

其中 $\lambda > 0$ 待定, $\bar{w}(k)$ 为外部输入, $\bar{z}(k)$ 为被控输出. 记

$$\bar{Q} = \begin{bmatrix} Q & 0 \\ 0 & -R_0 \end{bmatrix}, \quad \bar{S} = \begin{bmatrix} S & 0 \\ 0 & -S_0^T \end{bmatrix}, \quad \bar{R} = \begin{bmatrix} R & 0 \\ 0 & -Q_0 \end{bmatrix}.$$

我们有

定理3 给定矩阵 Q, S, R 且 Q, R 为对称的. 如果存在 $\lambda > 0$ 使系统(8)二次稳定且严格 $(\bar{Q}, \bar{S}, \bar{R})$ -耗散, 则在假设 A1), A2), A3), A4) 下系统(6)鲁棒稳定且严格 (Q, S, R) -耗散.

证 如果存在 $\lambda > 0$ 使系统(8)二次稳定且严格 $(\bar{Q}, \bar{S}, \bar{R})$ -耗散, 则存在 $P > 0, W > 0$ 使

$$\begin{bmatrix} -P + W & * & * & * & * \\ 0 & -W & * & * & * \\ -\bar{S}^T C_{1\lambda} & -\bar{S}^T C_{1d\lambda} & -D_{11\lambda}^T \bar{S} - \bar{S}^T D_{11\lambda} - \bar{R} & * & * \\ P A & P A_d & P B_{1\lambda} & -P & * \\ L C_{1\lambda} & L C_{1d\lambda} & L D_{11\lambda} & 0 & -I \end{bmatrix} < 0,$$

这里 $L^T L$ 为 $-\bar{Q}$ 的满秩分解.

将 $B_{1\lambda}, C_{1\lambda}, C_{1d\lambda}, D_{11\lambda}, \bar{Q}, \bar{S}, \bar{R}$ 代入并利用 Schur 补, 得

$$\begin{bmatrix} -C_1^T Q C_1 & * & * & * \\ -C_{1d}^T Q C_1 & -C_{1d}^T Q C_{1d} & * & * \\ -S^T C_1 - D_{11}^T Q C_1 & -S^T C_{1d} - D_{11}^T Q C_{1d} & -R - D_{11}^T S - S^T D_{11} - D_{11}^T Q D_{11} & * \\ -\lambda^{1/2} H_2^T Q C_1 & -\lambda^{1/2} H_2^T Q C_{1d} & -\lambda^{1/2} H_2^T Q D_{11} - \lambda^{1/2} H_2^T S & -\lambda H_2^T Q H_2 \end{bmatrix} +$$

$$\begin{bmatrix} \lambda^{-1} E_1^T R_0 E_1 & * & * & * \\ \lambda^{-1} E_{1d}^T R_0 E_1 & \lambda^{-1} E_{1d}^T R_0 E_{1d} & * & * \\ \lambda^{-1} E_2^T R_0 E_1 & \lambda^{-1} E_2^T R_0 E_{1d} & \lambda^{-1} E_2^T R_0 E_2 & * \\ \lambda^{-1/2} J^T R_0 E_1 + \lambda^{-1/2} S_0 E_1 & \lambda^{-1/2} J^T R_0 E_{1d} + \lambda^{-1/2} S_0 E_{1d} & \lambda^{-1/2} J^T R_0 E_2 + \lambda^{-1/2} S_0 E_2 & Q_0 + S_0 J + J^T S_0^T + J^T R_0 J \end{bmatrix} < 0,$$

以 $\text{diag}(I, I, I, \lambda^{-1/2}I)$ 对 Π 作合同变换,得

$$\bar{U} = \begin{bmatrix} -P + W + A^T P A & * & * & * \\ A_d^T P A & -W + A_d^T P A_d & * & * \\ B_1^T P A & B_1^T P A_d & B_1^T P B_1 & * \\ H_1^T P A & H_1^T P A_d & H_1^T P B_1 & H_1^T P H_1 \end{bmatrix} +$$

$$\begin{bmatrix} -C_1^T Q C_1 & * & * & * \\ -C_{1d}^T Q C_1 & -C_{1d}^T Q C_{1d} & * & * \\ -S^T C_1 - D_{11}^T Q C_1 & -S^T C_{1d} - D_{11}^T Q C_{1d} & -R - D_{11}^T S - S^T D_{11} - D_{11}^T Q D_{11} & * \\ -H_2^T Q C_1 & -H_2^T Q C_{1d} & -H_2^T Q D_{11} - H_2^T S & -H_2^T Q H_2 \end{bmatrix} +$$

$$\begin{bmatrix} \lambda^{-1} E_1^T R_0 E_1 & * & * & * \\ \lambda^{-1} E_{1d}^T R_0 E_1 & \lambda^{-1} E_{1d}^T R_0 E_{1d} & * & * \\ \lambda^{-1} E_2^T R_0 E_1 & \lambda^{-1} E_2^T R_0 E_{1d} & \lambda^{-1} E_2^T R_0 E_2 & * \\ \lambda^{-1} (J^T R_0 E_1 + S_0 E_1) & \lambda^{-1} (J^T R_0 E_{1d} + S_0 E_{1d}) & \lambda^{-1} (J^T R_0 E_2 + S_0 E_2) & \lambda^{-1} (Q_0 + S_0 J + J^T S_0^T + J^T R_0 J) \end{bmatrix} < 0.$$

取

$$\bar{V}(x(k)) = V(x(k)) + \lambda^{-1} (< \xi, Q_0 \xi >_{k-1} + 2 < \xi, S_0 \sigma >_{k-1} + < \sigma, R_0 \sigma >_{k-1}),$$

其中 $V(x(k)) = x^T(k) P x(k) + \sum_{l=k-d}^{k-1} x^T(l) W x(l)$.

记

$$\xi^T(k) = [x^T(k) \quad x^T(k-d) \quad w^T(k) \quad \xi^T(k)],$$

则

$$\begin{aligned} \Delta \bar{V} - z^T(k) Q z(k) - 2z^T(k) S w(k) - w^T(k) R w(k) = \\ \bar{V}(x(k+1)) - \bar{V}(x(k)) - z^T(k) Q z(k) - \\ 2z^T(k) S w(k) - w^T(k) R w(k) = \\ (Ax(k) + A_d x(k-d) + B_1 w(k) + \\ H_1 \xi(k))^T P (Ax(k) + A_d x(k-d) + B_1 w(k) + \\ H_1 \xi(k)) - x^T(k) P x(k) + x^T(k) W x(k) - \\ x^T(k-d) W x(k-d) + \lambda^{-1} \xi^T(k) Q_0 \xi(k) + \\ 2\lambda^{-1} \xi^T(k) S_0 (E_1 x(k) + E_{1d} x(k-d) + E_2 w(k) + \\ J \xi(k)) + \lambda^{-1} (E_1 x(k) + E_{1d} x(k-d) + E_2 w(k) + \\ J \xi(k))^T R_0 (E_1 x(k) + E_{1d} x(k-d) + E_2 w(k) + \end{aligned}$$

$$\begin{aligned} J \xi(k)) - w^T(k) R w(k) - 2(C_1 x(k) + C_{1d} x(k-d) + \\ D_{11} w(k) + H_2 \xi(k))^T S w(k) - (C_1 x(k) + \\ C_{1d} x(k-d) + D_{11} w(k) + H_2 \xi(k))^T Q (C_1 x(k) + \\ C_{1d} x(k-d) + D_{11} w(k) + H_2 \xi(k)) = \\ \xi^T(k) \bar{U} \xi(k) < 0, \forall \xi(k) \neq 0. \end{aligned}$$

从而存在 $\alpha > 0$ 使

$$\begin{aligned} \Delta V + \lambda^{-1} (\xi^T(k) Q_0 \xi(k) + 2\xi^T(k) S_0 \sigma(k) + \\ \sigma^T(k) R_0 \sigma(k)) - z^T(k) Q z(k) - 2z^T(k) S w(k) - \\ w^T(k) R w(k) + \alpha w^T(k) w(k) < 0. \end{aligned} \quad (9)$$

对 k 从 0 到 $K-1$ 求和并令

$$\beta(x_0) = x_0^T(0) P x_0(0) + \sum_{i=-d}^{-1} x_0^T(i) W x_0(i).$$

得

$$\begin{aligned} V(x, K) - \beta(x_0) + \lambda^{-1} (< \xi, Q_0 \xi >_{K-1} + 2 < \xi, \\ S_0 \sigma >_{K-1} + < \sigma, R_0 \sigma >_{K-1}) + \alpha < w, w >_{K-1} - < z, \\ Q z >_{K-1} - 2 < z, S w >_{K-1} - < w, Q w >_{K-1} < 0. \end{aligned}$$

当初始条件为零时,注意到(7)及 $V(x, K) \geq 0$ 可知

$$< z, Q z >_{K-1} + 2 < z, S w >_{K-1} +$$

$$\langle w, Qw \rangle_{K-1} \geq \alpha \langle w, w \rangle_{K-1}.$$

故系统(6)是严格\$(Q, S, R)\$-耗散的.

另外,令\$w(k) = 0\$,由(9)利用(7)得

$$\Delta V - z^T(k)Qz(k) < 0.$$

注意到假设A1)可知系统(6)是鲁棒稳定的.

定理3告诉我们,不确定系统(6)的鲁棒耗散分析问题可通过构造增广系统转化为确定系统的情形,运用这一思想也可解决这类不确定系统的鲁棒耗散控制问题.

4 鲁棒耗散控制(Robust dissipative control)

在系统(6)中引入控制项并添加量测方程,得

$$\begin{cases} x(k+1) = Ax(k) + A_d x(k-d) + B_1 w(k) + B_2 u(k) + H_1 \xi(k), \\ z(k) = C_1 x(k) + C_{1d} x(k-d) + D_{11} w(k) + D_{12} u(k) + H_2 \xi(k), \\ y(k) = C_2 x(k) + C_{2d} x(k-d) + D_{21} w(k) + H_3 \xi(k), \\ \sigma(k) = E_1 x(k) + E_{1d} x(k-d) + E_2 w(k) + E_3 u(k) + J \xi(k), \\ x(k) = x_0(k), -d \leq k \leq 0. \end{cases} \quad (10)$$

其中:\$u(k) \in \mathbb{R}^m\$为控制输入,\$y(k) \in \mathbb{R}^r\$为量测输出.\$B_2, D_{12}, E_3, C_2, C_{2d}, D_{21}, H_3\$为适当维数的已知矩阵.其余变量和矩阵与系统(6)的相同,特别是不确定变量\$\xi(k), \sigma(k)\$仍满足耗散不确定性条件(7).

现要设计\$n\$阶动态输出反馈

$$\begin{cases} x_c(k+1) = A_c x_c(k) + B_c y(k), \\ u(k) = C_c x_c(k). \end{cases} \quad (11)$$

使之与系统(10)构成的闭环系统是鲁棒稳定且严格\$(Q, S, R)\$-耗散的.为此,引入下面的增广系统

$$\begin{cases} x(k+1) = Ax(k) + A_d x(k-d) + B_{1\lambda} \bar{w}(k) + B_2 u(k), \\ \bar{z}(k) = C_{1\lambda} x(k) + C_{1d\lambda} x(k-d) + D_{11\lambda} \bar{w}(k) + D_{12\lambda} u(k), \\ y(k) = C_2 x(k) + C_{2d} x(k-d) + D_{21\lambda} \bar{w}(k). \end{cases} \quad (12)$$

其中\$D_{21\lambda} = [D_{21} \lambda^{1/2} H_3]\$, \$D_{12\lambda} = [D_{12}^T \lambda^{-1/2} E_3^T]^T\$. \$B_{1\lambda}, C_{1\lambda}, C_{1d\lambda}, D_{11\lambda}\$与系统(8)的相同.

下面的定理给出了本文的主要结果:

定理4 给定矩阵\$Q, S, R\$且\$Q, R\$为对称的,在假设A1),A2),A3),A4)下考虑系统(10).如果存在\$\lambda > 0\$使系统(12)与动态输出反馈(11)组成的闭环系统是二次稳定且严格\$(\bar{Q}, \bar{S}, \bar{R})\$-耗散的,则系统(10)与该动态输出反馈组成的闭环系统是鲁棒稳定且严格\$(Q, S, R)\$-耗散的.

证 系统(10)与动态输出反馈(11)组成的闭环系统为

$$\begin{cases} \eta(k+1) = \bar{A} \eta(k) + \bar{A}_d \eta(k-d) + \bar{B}_1 w(k) + \bar{H}_1 \xi(k), \\ z(k) = \bar{C}_1 \eta(k) + \bar{C}_{1d} \eta(k-d) + D_{11} w(k) + H_2 \xi(k), \\ \sigma(k) = \bar{E}_1 \eta(k) + \bar{E}_{1d} \eta(k-d) + E_2 w(k) + J \xi(k), \\ \eta(k) = \eta_0(k), -d \leq k \leq 0. \end{cases} \quad (13)$$

其中\$\eta(k) = [x^T(k) \ x_c^T(k)]^T\$,

$$\bar{A} = \begin{bmatrix} A & B_2 C_c \\ B_c C_2 & A_c \end{bmatrix}, \bar{A}_d = \begin{bmatrix} A_d & 0 \\ B_c C_{2d} & 0 \end{bmatrix}, \bar{B}_1 = \begin{bmatrix} B_1 \\ B_c D_{21} \end{bmatrix}.$$

$$\bar{H}_1 = \begin{bmatrix} H_1 \\ B_c H_3 \end{bmatrix}, \bar{C}_1 = [C_1 \ D_{12} C_c], \bar{C}_{1d} = [C_{1d} \ 0],$$

$$\bar{E}_1 = [E_1 \ E_3 C_c], \bar{E}_{1d} = [E_{1d} \ 0].$$

系统(12)与动态输出反馈(11)组成的闭环系统为

$$\begin{cases} \eta(k+1) = \bar{A} \eta(k) + \bar{A}_d \eta(k-d) + [\bar{B}_1 \ \lambda^{1/2} \bar{H}_1] \bar{w}(k), \\ \bar{z}(k) = \begin{bmatrix} \bar{C}_1 \\ \lambda^{-1/2} \bar{E}_1 \end{bmatrix} \eta(k) + \begin{bmatrix} \bar{C}_{1d} \\ \lambda^{-1/2} \bar{E}_{1d} \end{bmatrix} \eta(k-d) + \begin{bmatrix} D_{11} & \lambda^{1/2} H_2 \\ \lambda^{-1/2} E_2 & J \end{bmatrix} \bar{w}(k). \end{cases} \quad (14)$$

对系统(13),(14)应用定理3即得定理4的结论.

由定理3和定理4,不确定系统(10)的鲁棒耗散分析和动态输出反馈控制问题均可转化为确定系统的耗散分析和动态输出反馈控制,而后者可分别根据定理1,定理2求解.

5 仿真示例(Numerical example)

设系统(10)的参数为

$$A = \begin{bmatrix} 0.1 & 0.1 \\ 0 & -0.2 \end{bmatrix}, A_d = \begin{bmatrix} 0.1 & 0 \\ 0 & 0.1 \end{bmatrix},$$

$$B_1 = \begin{bmatrix} 0.1 \\ 0.1 \end{bmatrix}, B_2 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, H_1 = \begin{bmatrix} 0.1 \\ 0.05 \end{bmatrix},$$

$$C_1 = [0.1 \ 0.1], C_{1d} = [0.05 \ 0.01],$$

$$D_{11} = 0.1, D_{12} = 0.5, H_2 = 0.01,$$

$$C_2 = \begin{bmatrix} 1 & -0.1 \\ 0 & 0.5 \end{bmatrix}, C_{2d} = \begin{bmatrix} 0.1 & 0.1 \\ 0 & 0.1 \end{bmatrix},$$

$$C_{21} = \begin{bmatrix} 0.1 \\ 0 \end{bmatrix}, H_3 = \begin{bmatrix} -0.1 \\ 0.3 \end{bmatrix},$$

$$E_1 = [0.12 \ 0.01], E_{1d} = [0.1 \ 0.11],$$

$$E_2 = 0.2, E_3 = -0.2, J = 0.3.$$

关于该系统的不确定变量,假设\$\xi(k) = f(k)\sigma(k)\$

($|f(k)| \leq 1$), 即有 $Q_0 = -1$, $S_0 = 0$, $R_0 = 1$ 使(7)成立, 而且满足假设 A3), A4).

给定 $Q = -1$, $S = 1$, $R = 0.5$, 显然假设 A1), A2) 成立. 取 $\lambda = 1$, 将以上参数代入(12), 对这样得到的系统使用定理2 研究其输出反馈严格($\bar{Q}$, $\bar{S}$, $\bar{R}$)-耗散性.

对于 $W = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$, 借助于 Matlab 中的 LMI 工

具箱, 对相应矩阵不等式(3)求解, 得可行解

$$X = \begin{bmatrix} 0.8455 & -0.0151 \\ -0.0151 & 0.8458 \end{bmatrix}, Y = \begin{bmatrix} 2.3831 & 0.0081 \\ 0.0081 & 2.3681 \end{bmatrix},$$

$$H = \begin{bmatrix} 0.0526 & 0.0908 \\ -0.0143 & -0.1507 \end{bmatrix}, F = \begin{bmatrix} -0.1682 & -0.2999 \\ -0.0311 & 0.3766 \end{bmatrix},$$

$$G = \begin{bmatrix} -0.0296 & 0.0119 \end{bmatrix}.$$

由(4)通过奇异值分解求出

$$M = \begin{bmatrix} -0.7794 & -0.6265 \\ -0.6265 & 0.7794 \end{bmatrix}, N = \begin{bmatrix} 1.4557 & 1.0935 \\ 1.1699 & -1.3637 \end{bmatrix}.$$

根据(5)解得

$$A_c = \begin{bmatrix} -0.0472 & -0.0264 \\ 0.0299 & -0.0198 \end{bmatrix}, B_c = \begin{bmatrix} -12.3639 & -0.0653 \\ 2.0816 & -3.6095 \end{bmatrix},$$

$$C_c = \begin{bmatrix} 0.0156 & 0.0278 \end{bmatrix}.$$

由定理4, 由此确定的控制器(11)必使上述不确定系统鲁棒稳定且关于 $Q = -1$, $S = 1$, $R = 0.5$ 严格耗散.

6 结论(Conclusions)

本文讨论线性离散时滞系统的输出反馈二次型耗散控制问题, 研究了一类耗散不确定系统的鲁棒耗散分析和动态输出反馈鲁棒耗散设计问题, 结果表明鲁棒耗散分析和控制可转化为确定系统的情形. 所得结果可为线性离散时滞系统的 H_∞ 控制和无源控制提供统一的框架, 也可看作线性离散系统二次型耗散控制的推广.

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作者简介:

邵汉永 (1964—), 男, 博士, 研究领域为无源性分析, 自适应控制, 鲁棒控制, E-mail: hanyongshao@163.com.